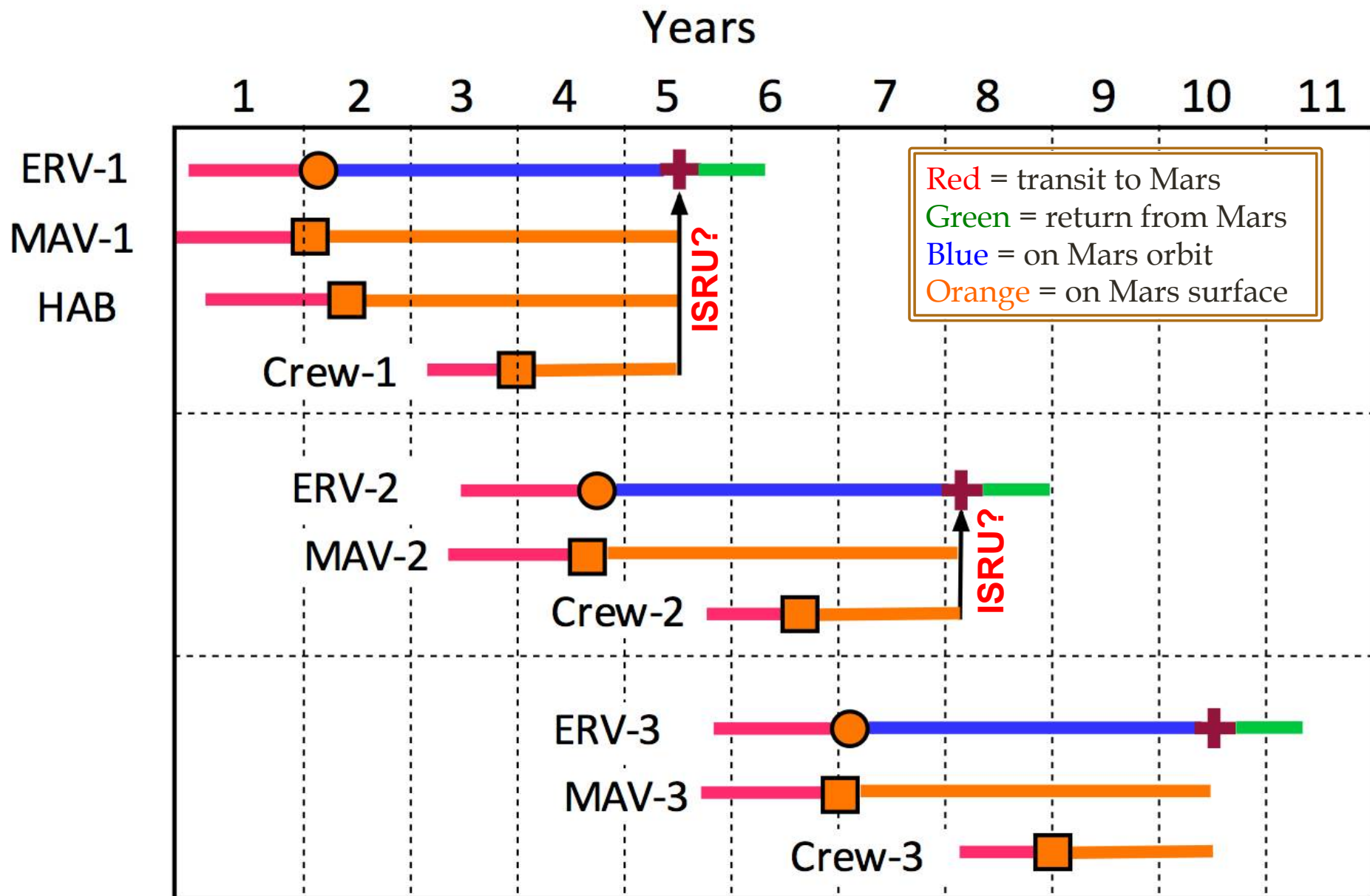




# Reference technology

(Mostly MOXIE)

# Long Term Mission Sequence





# Benefits of ISRU propellant



| ELEMENT                                                             | DRM-1<br>(mT) | DRM-3<br>(mT) | COMMENT                                           |
|---------------------------------------------------------------------|---------------|---------------|---------------------------------------------------|
| Ascent capsule                                                      | 4             | 6             | Includes crew of 6                                |
| Ascent propulsion stage                                             | 3             | 5             | Typically 15% of propellant requirement           |
| Propellant (CH <sub>4</sub> + O <sub>2</sub> )                      | 26            | 39            |                                                   |
| Mass saved in LEO if ISRU produces CH <sub>4</sub> + O <sub>2</sub> | 300 -500      | 440-800       | Depends on assumptions re: aerocapture/propulsion |
| Mass saved in LEO if ISRU produces only O <sub>2</sub>              | 230-380       | 330-620       | Depends on assumptions re: aerocapture/propulsion |

# Robotic ISRU: Make vs “buy”



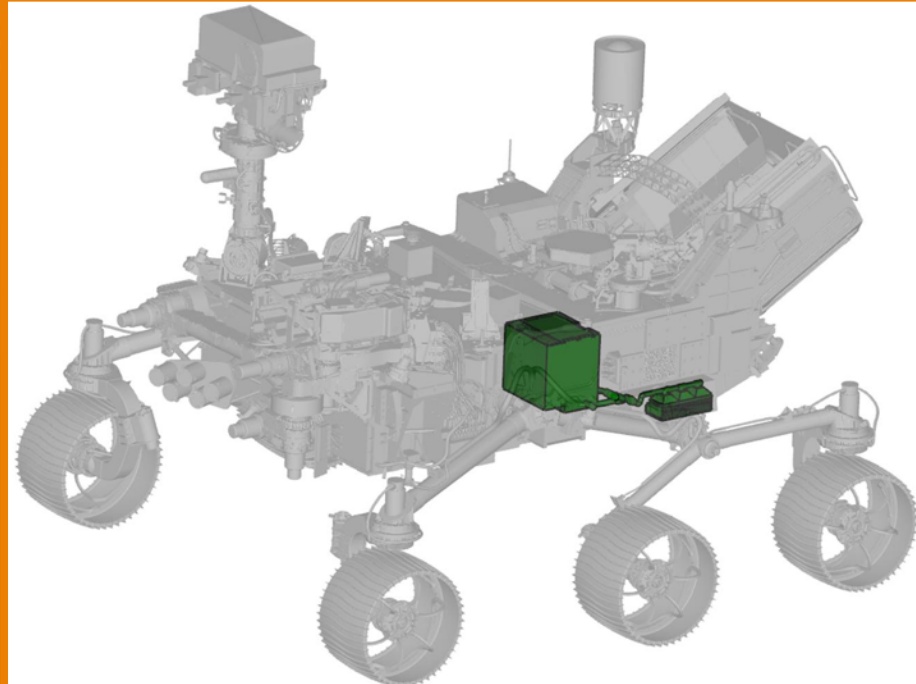
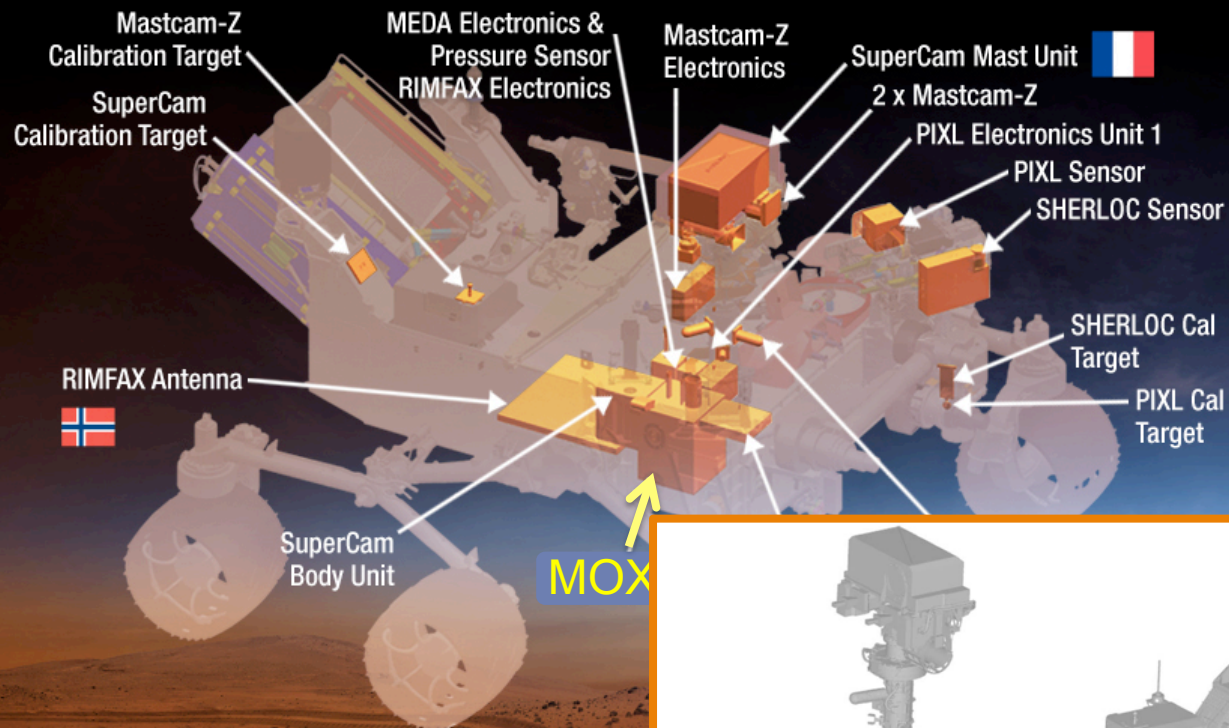
- \* Assumptions:
  - \* >25 kW power source
  - \* >12 months to produce propellant
- \*  $\text{CO}_2 \rightarrow \text{O}_2$ 
  - \* Mass: ~1 mT for system saves ~25 mT transported
  - \* Constraints imposed on mission: None
- \*  $\text{H}_2\text{O} + \text{CO}_2 \rightarrow \text{CH}_4$  (additional)
  - \* Mass: ~0.7 mT for system saves ~7 mT transported
  - \* Constraints imposed on mission:
    - \* Landing where water is available
    - \* Robotic prospecting, excavation, testing

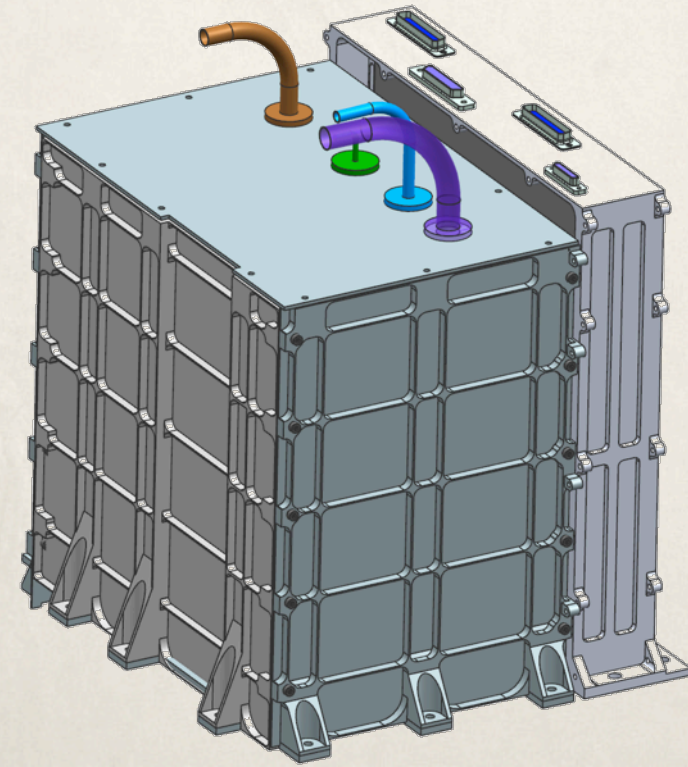
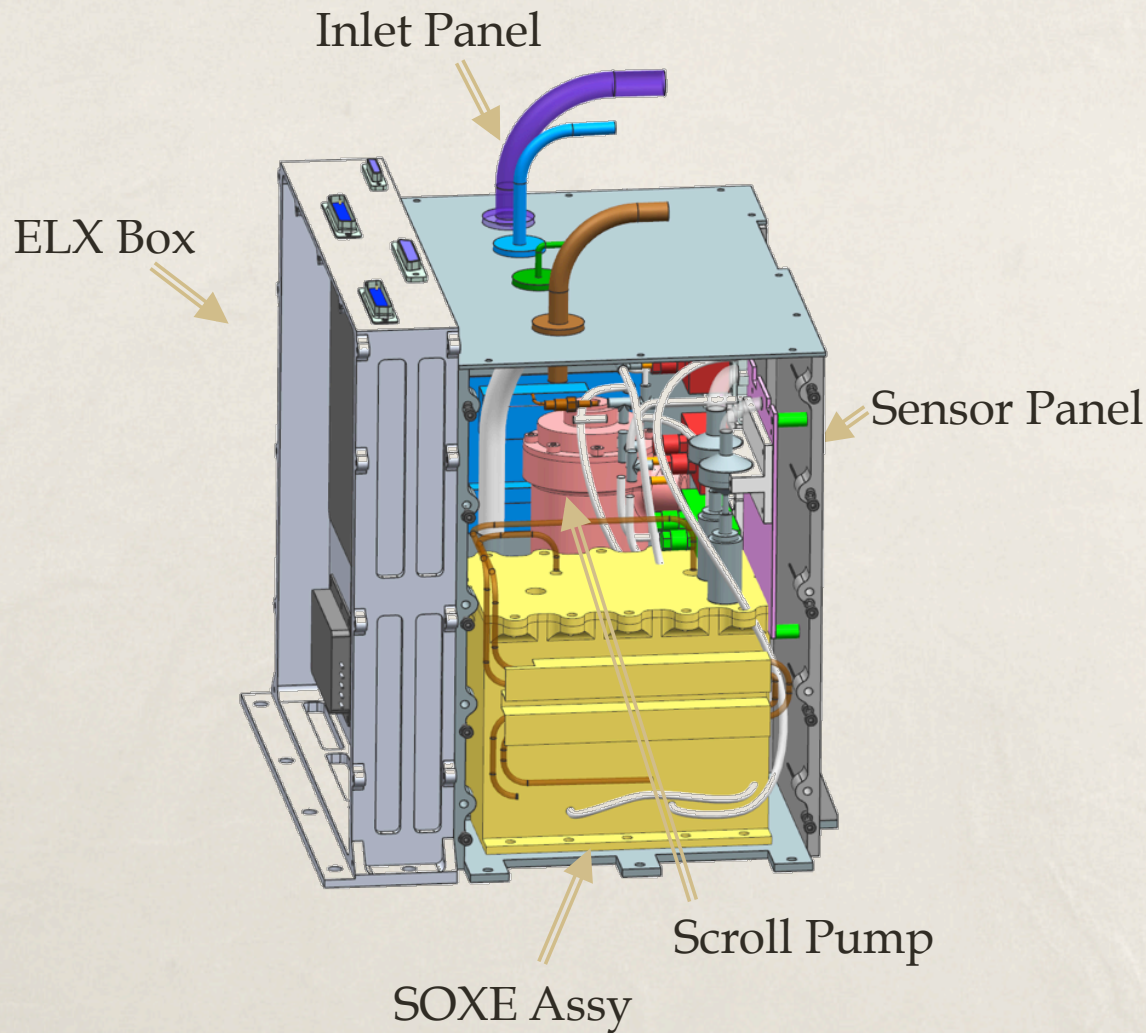
| Scenario  | Propellant-related S/C Mass (mT) |      |     |       |              | Propellant Produced (mT) | Figures of merit (n:1)      |                                   | Other considerations  |                          |                        |
|-----------|----------------------------------|------|-----|-------|--------------|--------------------------|-----------------------------|-----------------------------------|-----------------------|--------------------------|------------------------|
|           | ISRU h/w                         | O2   | CH4 | Total | Mass Savings |                          | Mass savings: ISRU h/w mass | Production: ISRU-related s/c mass | Requires excavation ? | Constrains landing site? | Flight-like prototype? |
| No ISRU   | 0                                | 24.6 | 7   | 31.6  |              | 0                        |                             |                                   |                       |                          |                        |
| LOx only  | 1                                | 0    | 7   | 8     | 24           | 24.6                     | 24                          | 3                                 | No                    | No                       | Yes                    |
| LOx + CH4 | 1.7                              | 0    | 0   | 1.7   | 30           | 31.6                     | 18                          | 19                                | Yes                   | Yes                      | No                     |

Source: M-WIP study



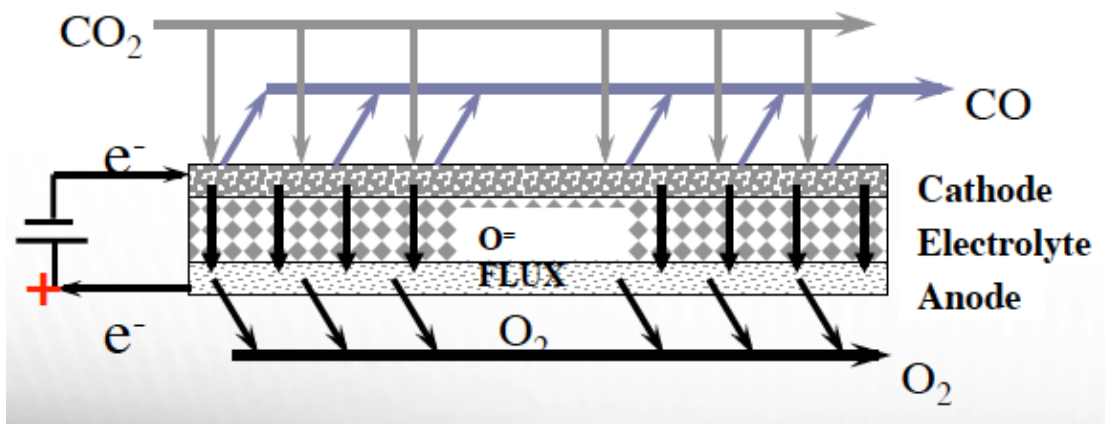
# Mars 2020 Rover



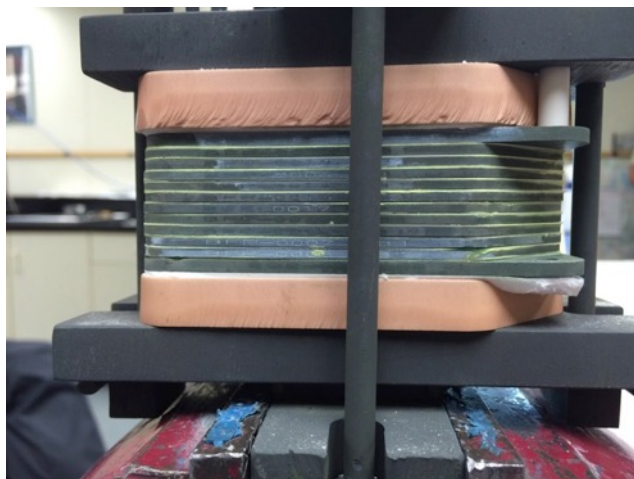


- ~1:200 scale production
- ~1:400 scale operating time
- No product storage
- No fuel production

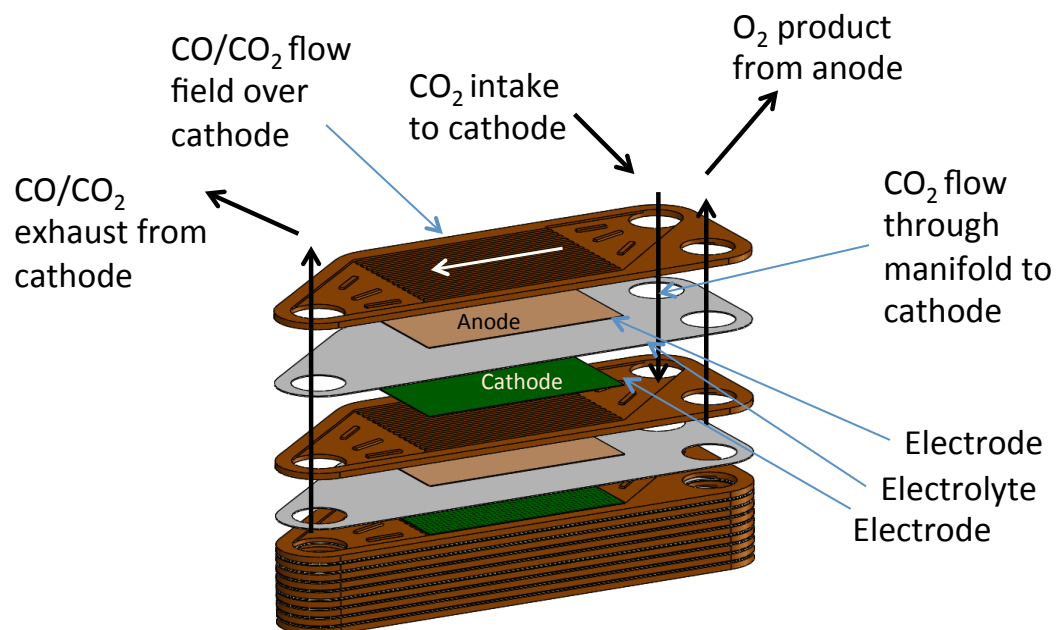




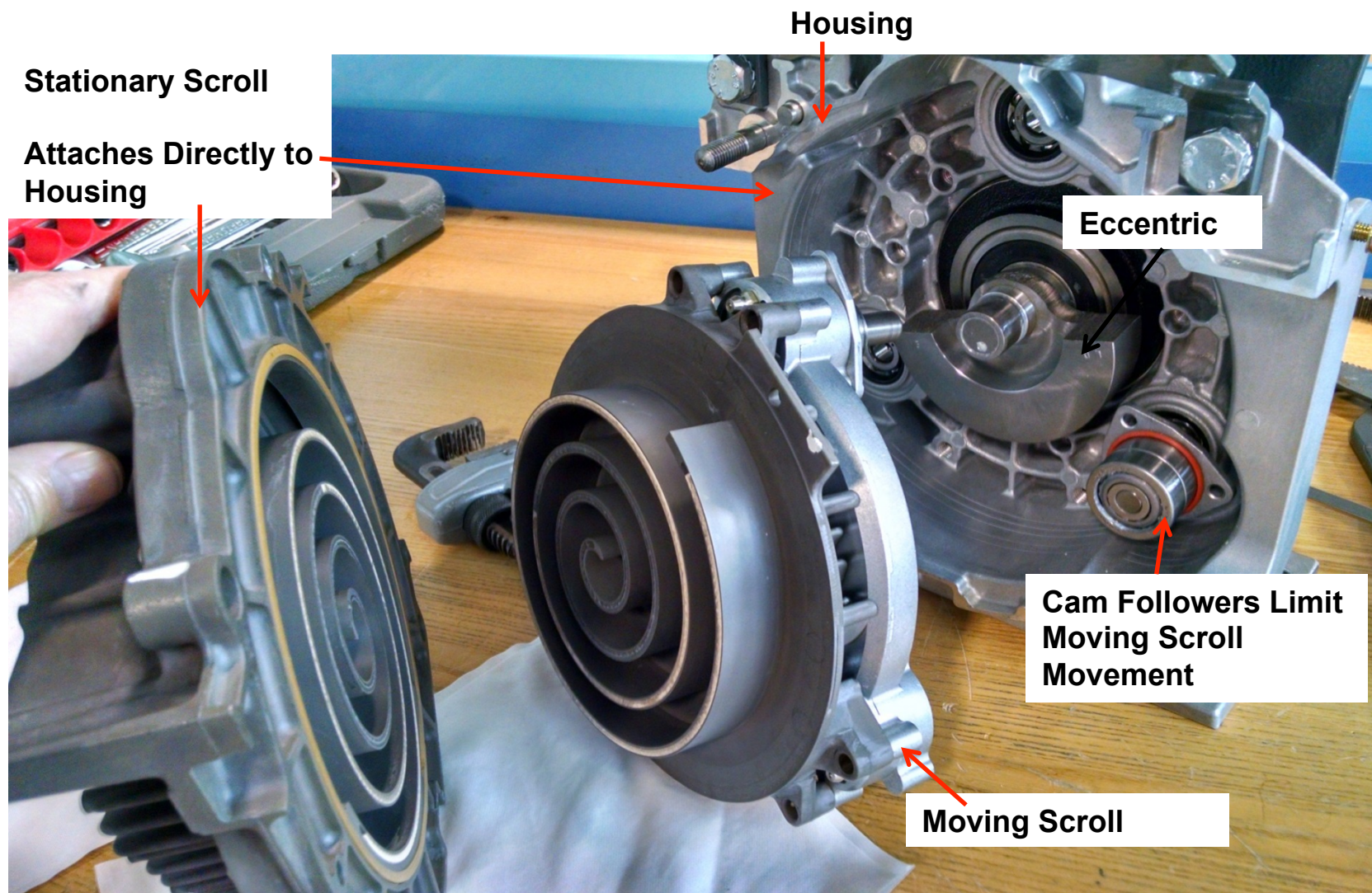
**SOXE**



SOXE 11 cell stack fabricated by  
Ceramatec



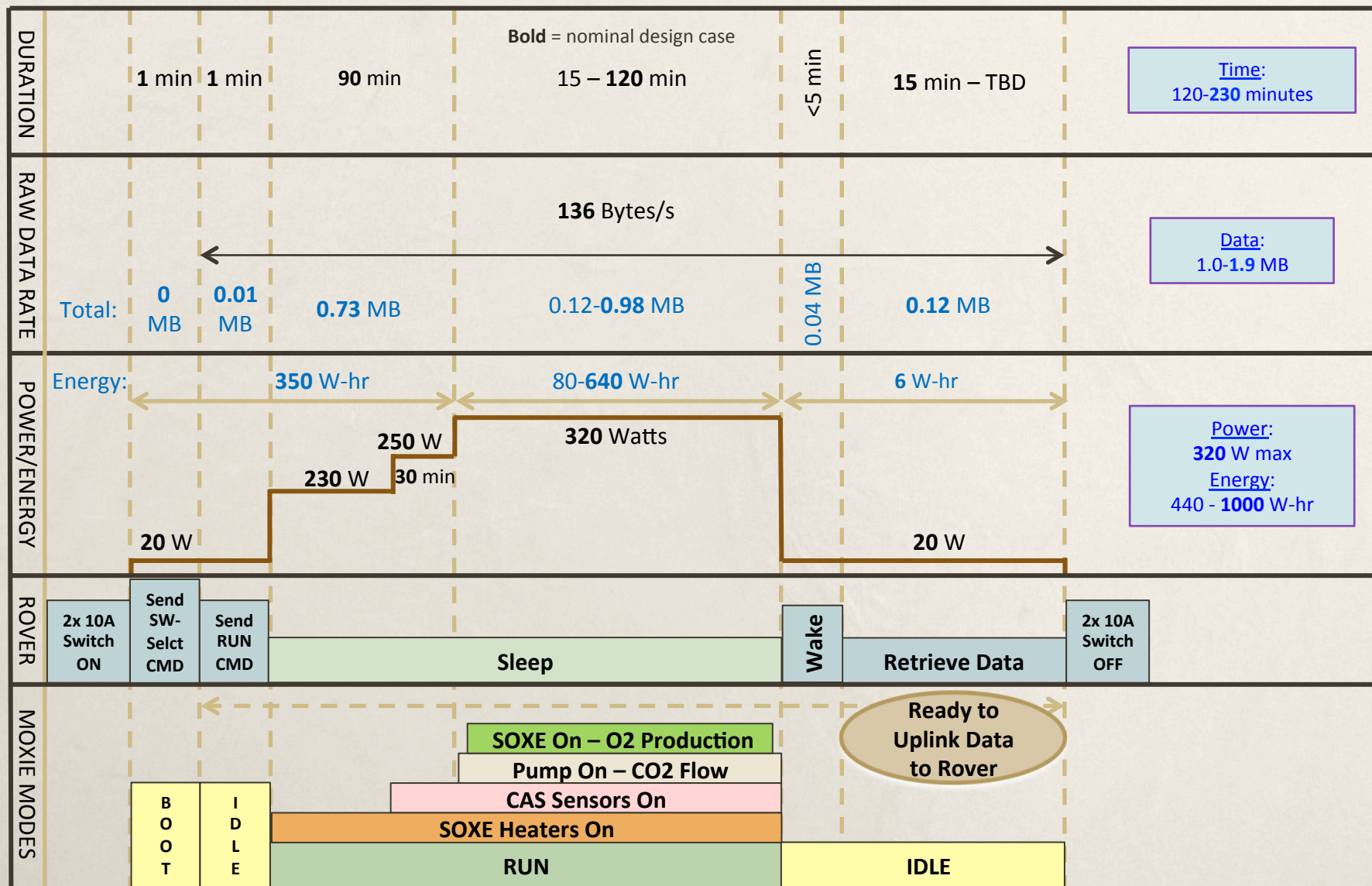
# Scroll pump



- Alternatives: Cryogenic, sorption bed



# Day in the Life



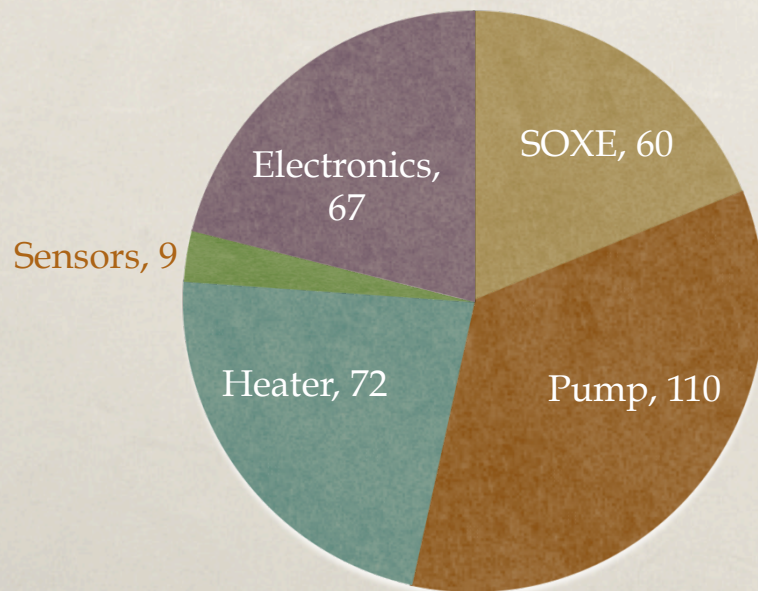
# Where does the power go?



|                                         |      |
|-----------------------------------------|------|
| * SOXE current:                         | 60W  |
| * Pump:                                 | 110W |
| * Stack heaters (mostly make-up heat):  | 72W  |
| * Sensors, incl. panel heating:         | 9W   |
| * Electronics, mostly DC/DC conversion: | 67W  |

**Total**

**320W**





# 2024 ISRU Validation w/ MSR option



## Concept:

Leveraging MOXIE, a 2024 validation mission to:

- Demonstrate end-to-end resource utilization and validation
- Launch a 6U CubeSat MAV payload with sample receptacle from Mars to elliptical orbit
- Offer option for delivery of Mars 2020 sample

## Technologies to be demonstrated:

- Precision Landing of  $>> 1$  mT, possibly SRP
- 1 kW power system (nuclear or solar)
- ISRU  $O_2$  generation ( $>5x$  break-even)
- Mars Ascent Vehicle (MAV)
- Cryogenic  $O_2$  storage and transfer to MAV
- Sample transfer to MAV
- MAV ascent to (elliptical) orbit
- Cubesat w/ station-keeping in Mars orbit
- Possible MAV propulsion (solar or SEP) to raise MAV orbit or return to Earth

## Rough numbers:

- |                          |                           |
|--------------------------|---------------------------|
| • ISRU System mass       | 21 kg                     |
| • ISRU Power             | 1067 W                    |
| • $O_2$ production rate  | 50 g/hr                   |
| • Time to generate $O_2$ | 89 sols                   |
|                          |                           |
| • MAV dry mass           | 24 kg                     |
| • MAV payload mass       | 12 kg                     |
| • $CH_4$ mass            | 31 kg                     |
| • ISRU $O_2$ mass        | 109 kg (5.2x system mass) |

## Notional Mission Timeline:

### **March, 2021:**

- Mars 2020 arrives at Mars

### **July 2024:**

- End Mars 2020 primary mission
- ISRU Mission Launches

### **March 2025:**

- ISRU Mission Lands

### **June 2025:**

- Complete ISRU MAV Fueling
- [Optional] Mars 2020 sample transfer
- MAV Launch

### **December 2026:**

- End ISRU Primary Mission

# What limits O<sub>2</sub> production?



## 1. Inlet flow

- \* Together with CO<sub>2</sub> utilization fraction, determines O<sub>2</sub> production
- \* Limited by overall pump capability
- \* Limited by inlet gas density, which is determined by:
  - \* **Ambient pressure & temperature**
  - \* **Pressure drop across filter, including dust**

## 2. Available power

- \* **Safe current limit of 4A**
- \* Power limit of 35W per supply (not normally a constraint)
- \* Circuit limit of 10A (not normally a constraint)
- \* Thermal constraints at high power (depends on many factors)

## 3. SOXE capability

- \* All the electrochemistry is captured in one empirical number, **ASR**, and a more-or-less constant number, OCV
- \* Scale by area (22.7 cm<sup>2</sup> and number of cells (5x2=10)
- \* Limited by **safe operating voltage and % CO<sub>2</sub> utilization**, largely TBD

*How do these factors rank in importance?*



# SOXE Challenges

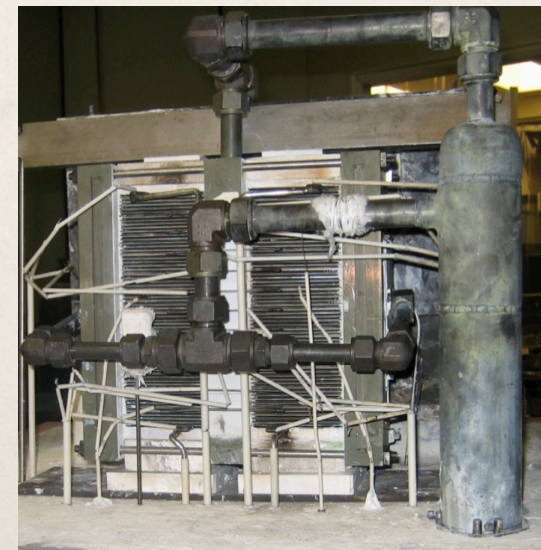
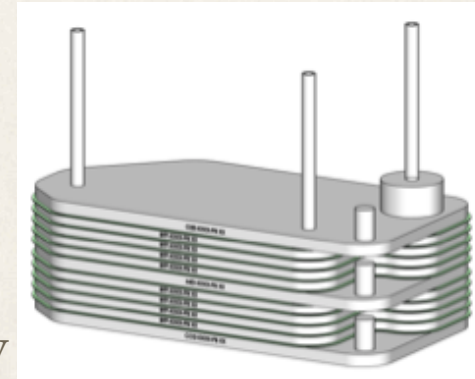


CERAMATEC  
TOMORROW'S CERAMIC SYSTEMS

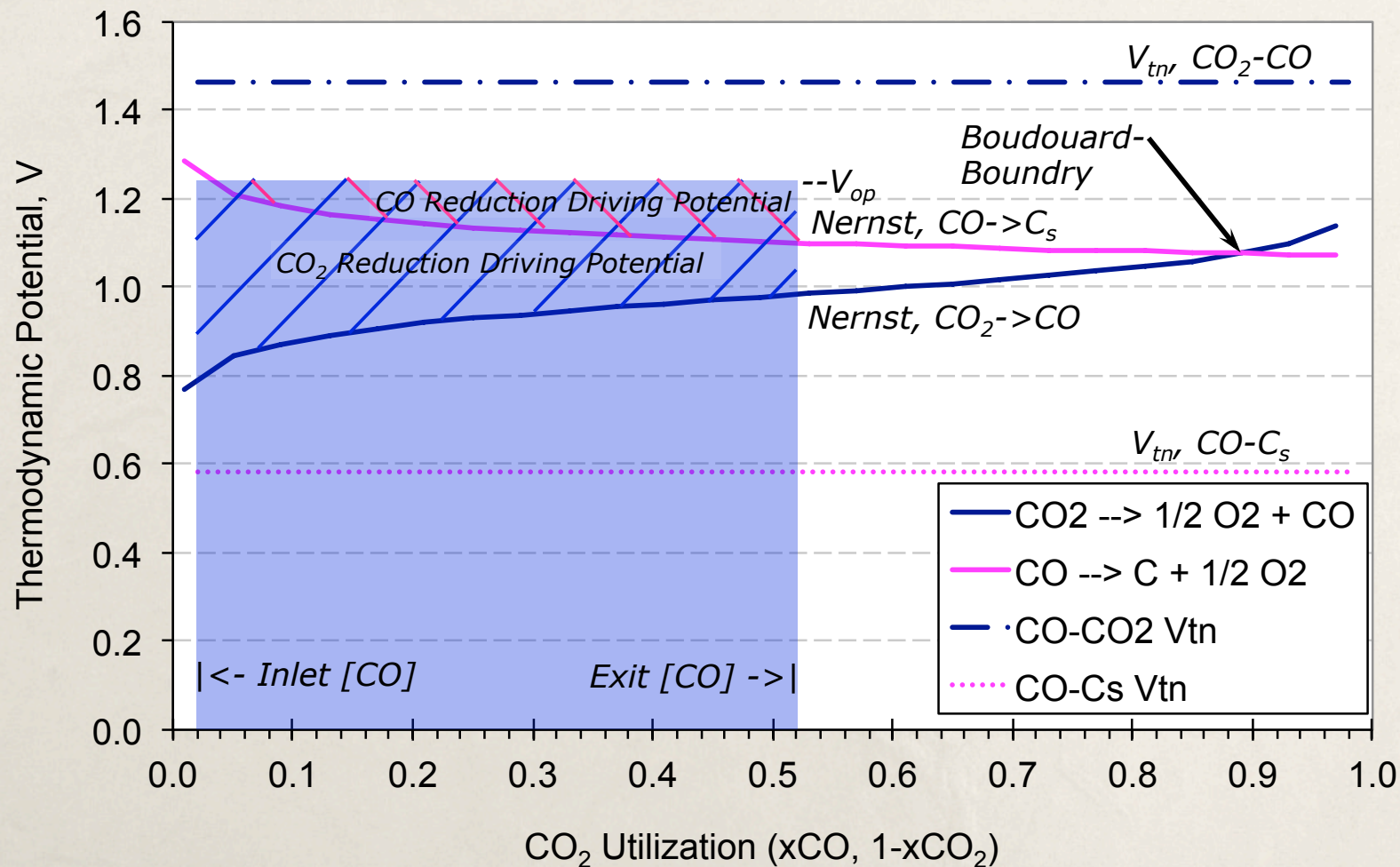


Mars 2020 Project

- \* Challenges & approaches
  - \* Dry CO<sub>2</sub> electrolysis
    - \* Custom materials
  - \* Heat/cool cycling
    - \* Controlled startup/shutdown; CTE matching
    - \* Cold-side compression to minimize pre-heat energy
  - \* Oxidation
    - \* CO recirculation
  - \* Coking
    - \* Limit on operating voltage
  - \* Low pressure environment
    - \* Hermetic (glass) sealing to formed interconnect
    - \* Compression fixture
  - \* Shock & vibration
    - \* Isolation mounting if needed
- \* Under development by Ceramatec, Inc. (a division of CoorsTek)



# $V_{op}$ Limited by CO Reduction Potential





# SOXE Summary



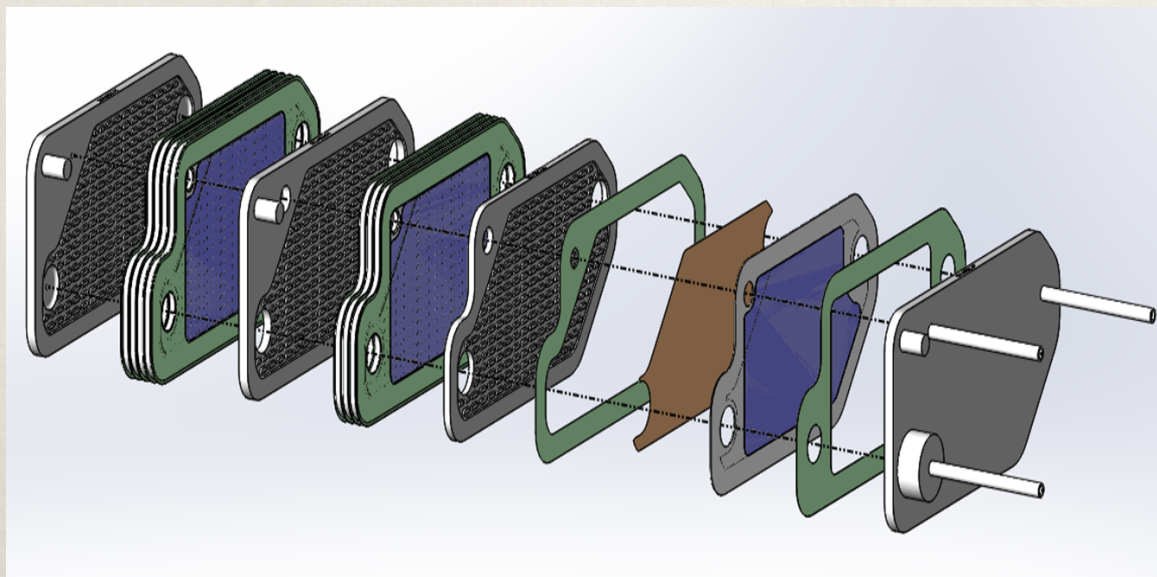
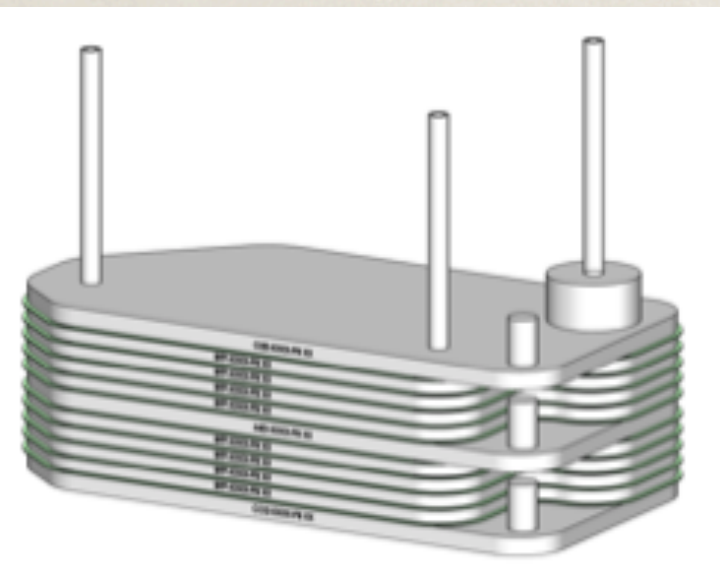
Mars 2020 Project

## ★ Results & Findings:

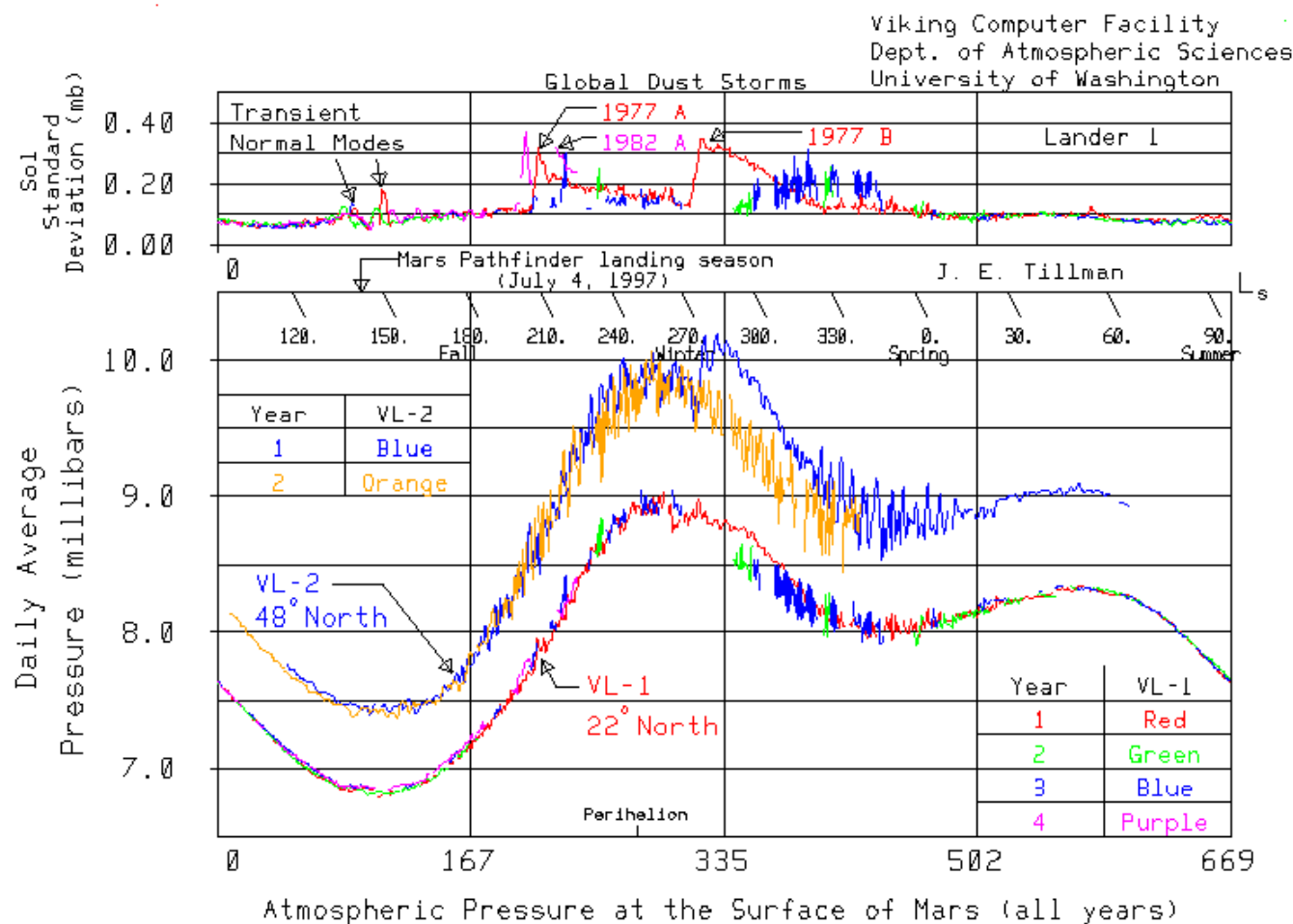
- ★ Low ASRs (2-2.5)
- ★ Stable to heat/cool cycling
- ★ Oxidation is a bigger challenge than coking
- ★ SOXE capability exceeds MOXIE resources on Mars

## ★ Still to be studied:

- ★ Limits on CO<sub>2</sub> utilization, voltage, temperature
- ★ Long-term performance (>1000 hrs)

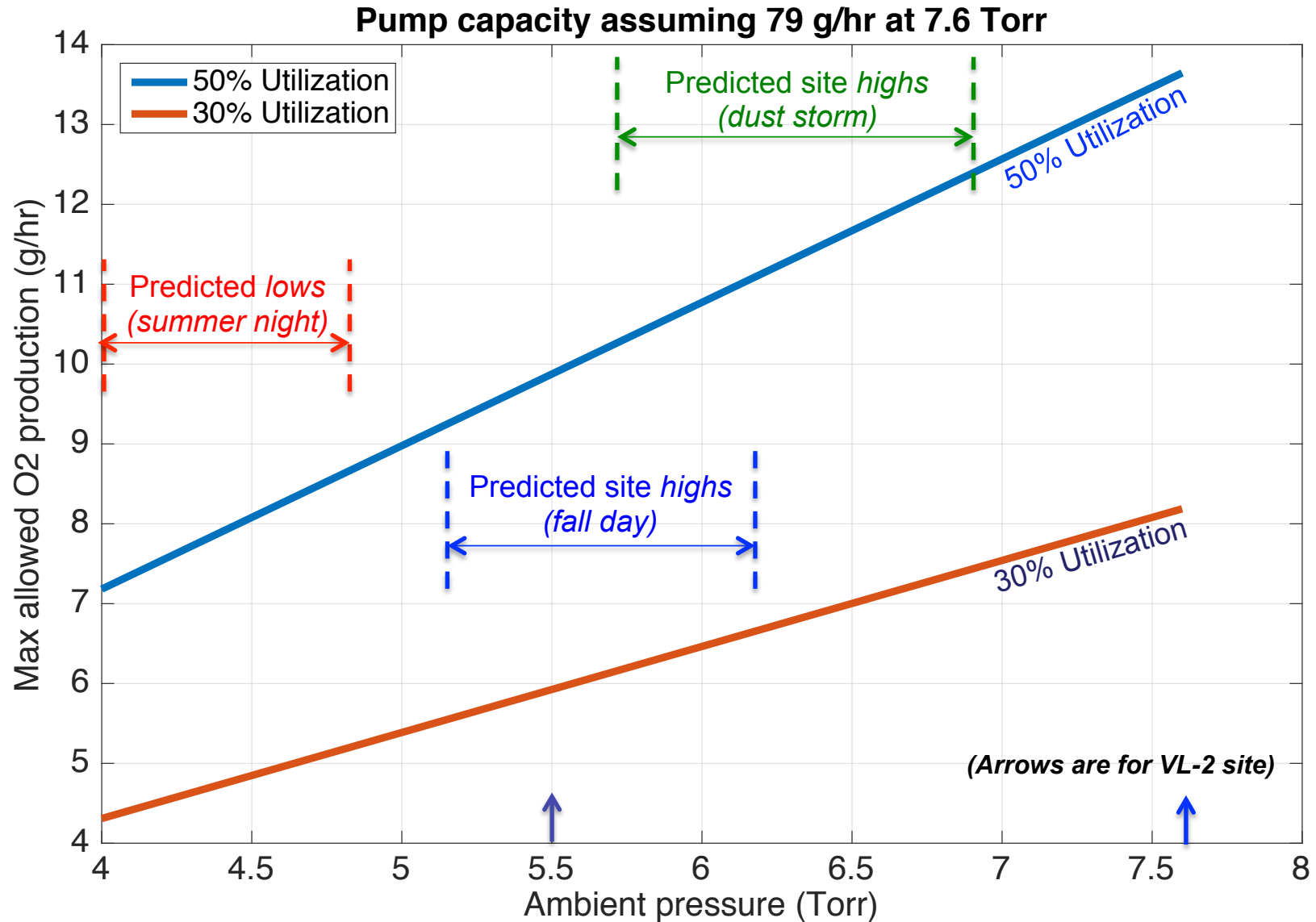


# Viking Pressure Data

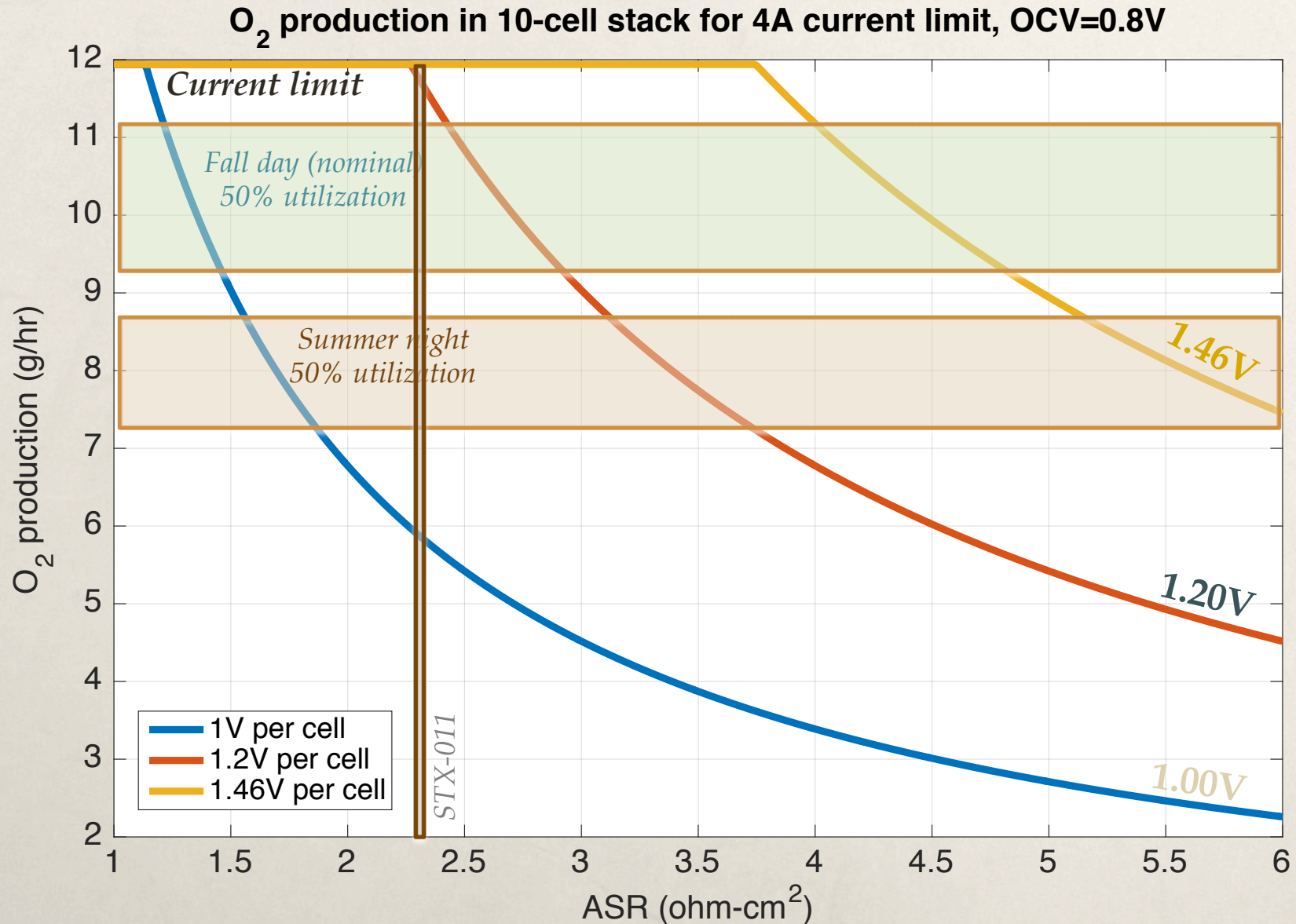




# Pump capacity (at 20°C inlet)

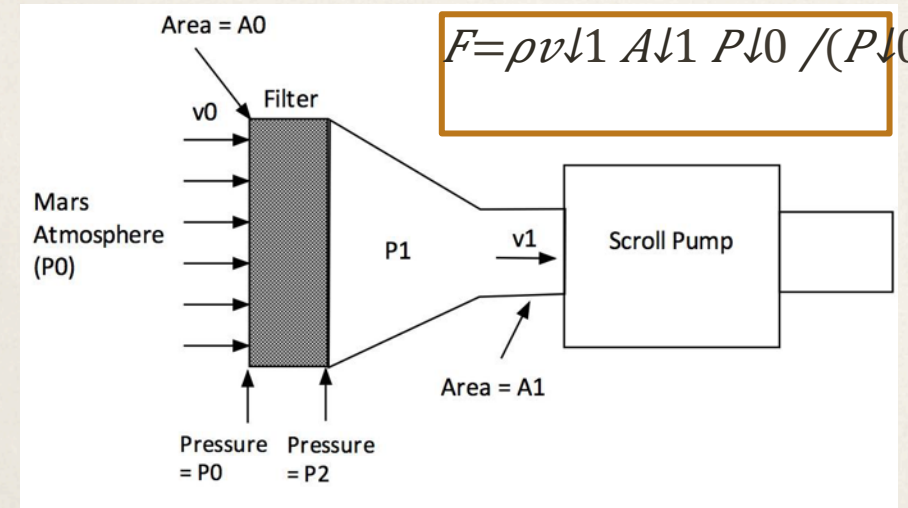
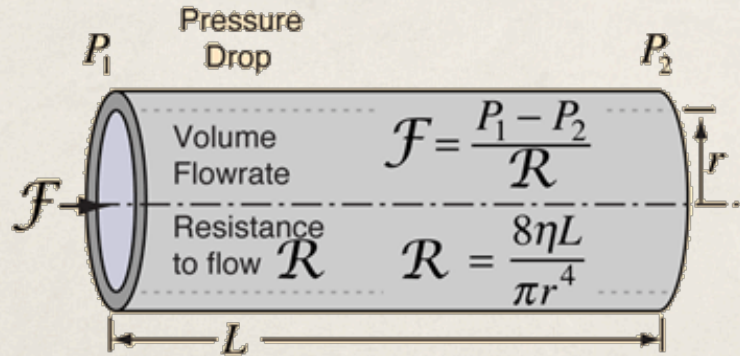


# SOXE Performance v. ASR

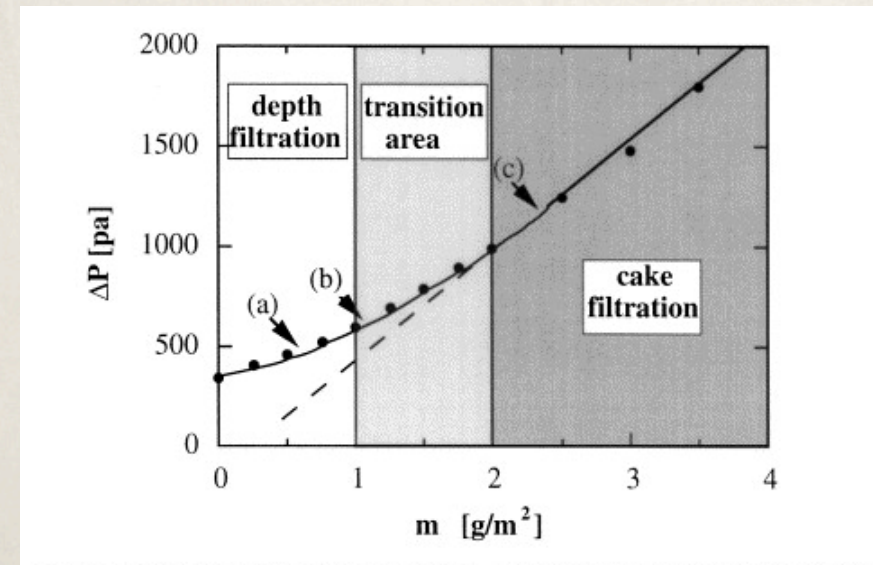




# Filter sensitivity to dust



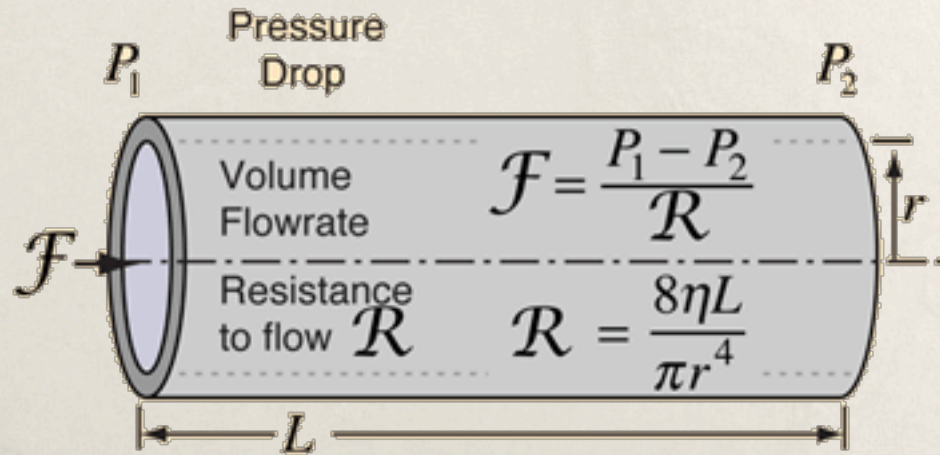
- ★ MOXIE will ingest  $\sim 50$  mg dust through a  $264 \text{ cm}^2$  *pleated* filter, or  $\sim 2 \text{ g/m}^2$ .
- ★ Incident velocity  $v_0$  typically  $\sim 5 \text{ cm/s}$ , comparable to Thomas study (right), but particles are typically larger.
- ★ Begin to get in trouble between  $1$ - $10 \text{ g/m}^2$
- ★ Full-scale MOXIE will ingest  $\sim 5 \text{ kg}$  dust over 1 year
- ★ Dust storms result in up to  $\times 10$  deposition.



$v_0 = 5 \text{ cm/s}$ ,  $d_p = 0.15 \mu\text{m}$ . From D. Thomas et al. (1999) *J. Aero. Sci.*, 30 (2), 235-246.

# Dust conclusions

- \* → Filters need to have huge surface area if they are not to obstruct flow, and are degraded by a few microns of dust
- \* The way forward?
  - \* Filter-less first-stage pumping?
  - \* Cyclone or electrostatic mitigation?



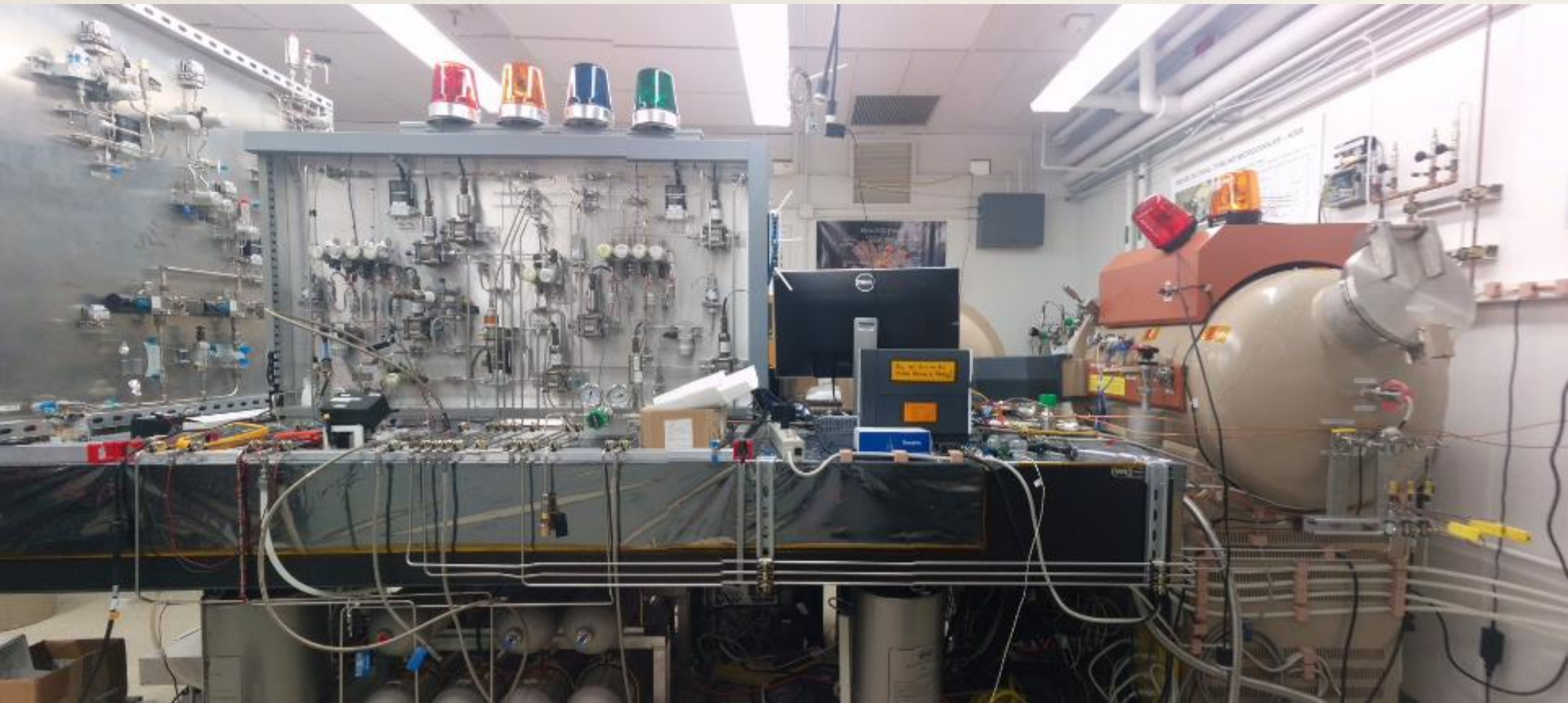


# Take-aways



- \* MOXIE production rate is determined by a number of factors, including:
  - \* SOXE capability
  - \* Pump capability
  - \* Power supply capability
  - \* Safe operating conditions (TBD)
  - \* Landing site & weather
  - \* Filtering and dust
- \* It is not currently expected that overall O<sub>2</sub> production will be limited by SOXE performance. This is probably typical of reference systems.

*Special thanks to the amazing JPL Project Team!*



*MOXIE Testbed*



M. Hecht, MIT/HO (PI)

J. Hoffman, MIT (DPI)

G. Sanders, JSC

D. Rapp, Consultant

B. Yildiz, MIT

G. Voecks, JPL

K. Lackner, ASU

J. Hartvigsen, Ceramatec

P. Smith, Space Expl. Instr.

W. T. Pike, Imperial Coll.

M. Madsen, U. Copen.

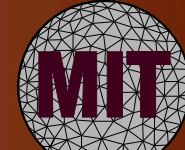
C. Graves, DTU (Coll.)

M. de la Torre Juarez, JPL (Coll.)



Jet Propulsion Laboratory  
California Institute of Technology

J. Mellstrom, Project Manager



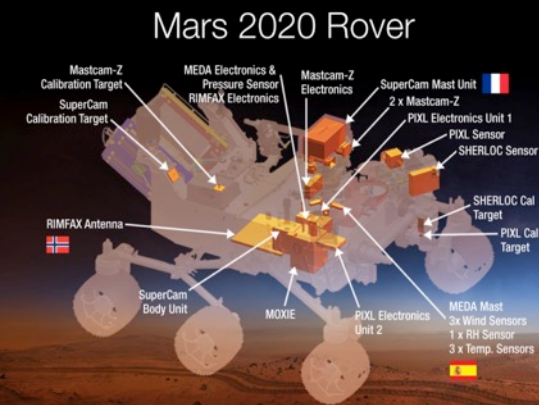
HAYSTACK OBSERVATORY

# MOXIE

## The Mars Oxygen ISRU Experiment On NASA's Mars 2020 Rover

A joint project of NASA's:

- HEOMD
- STMD
- SMD

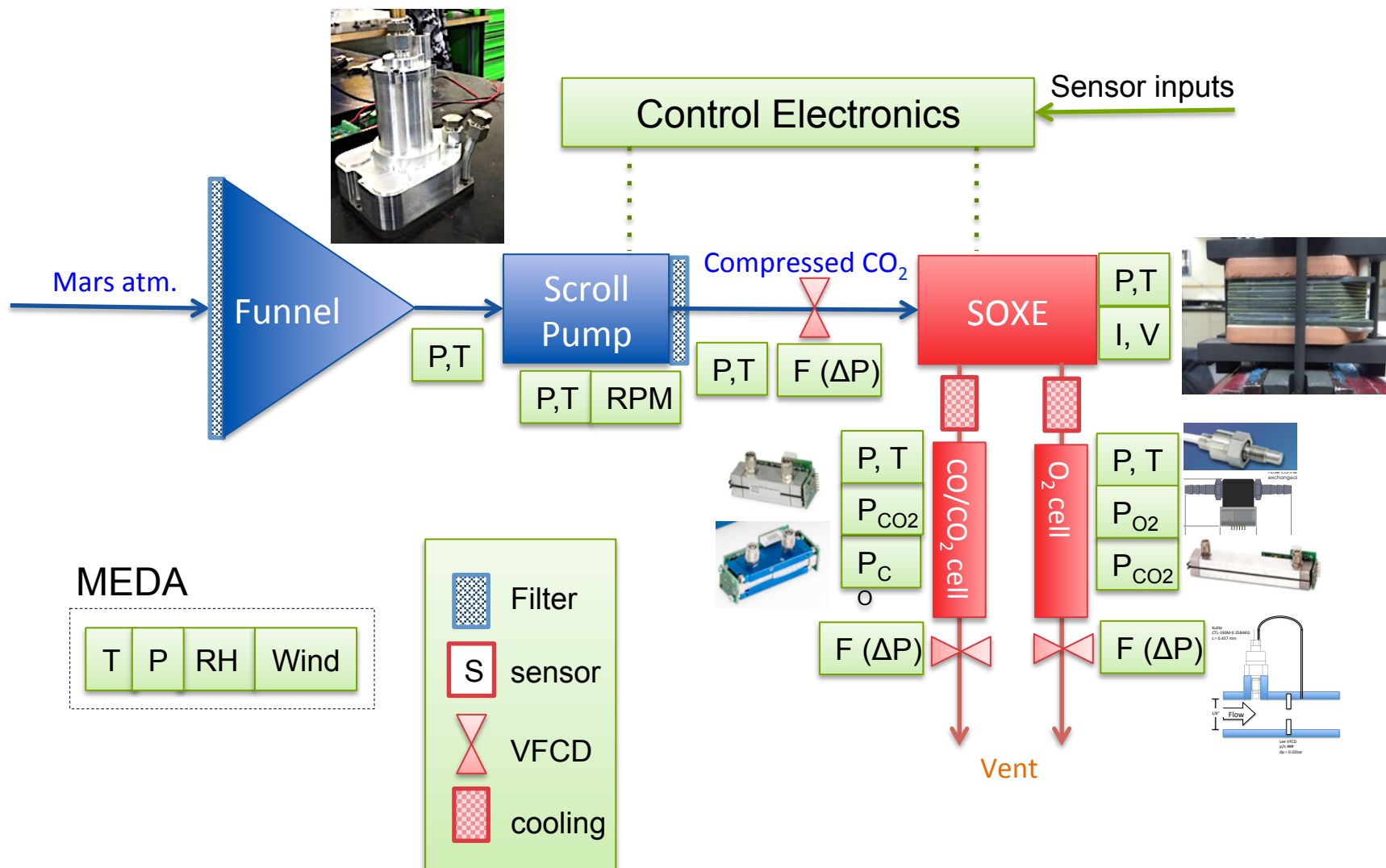




# More MOXIE

Backup slides

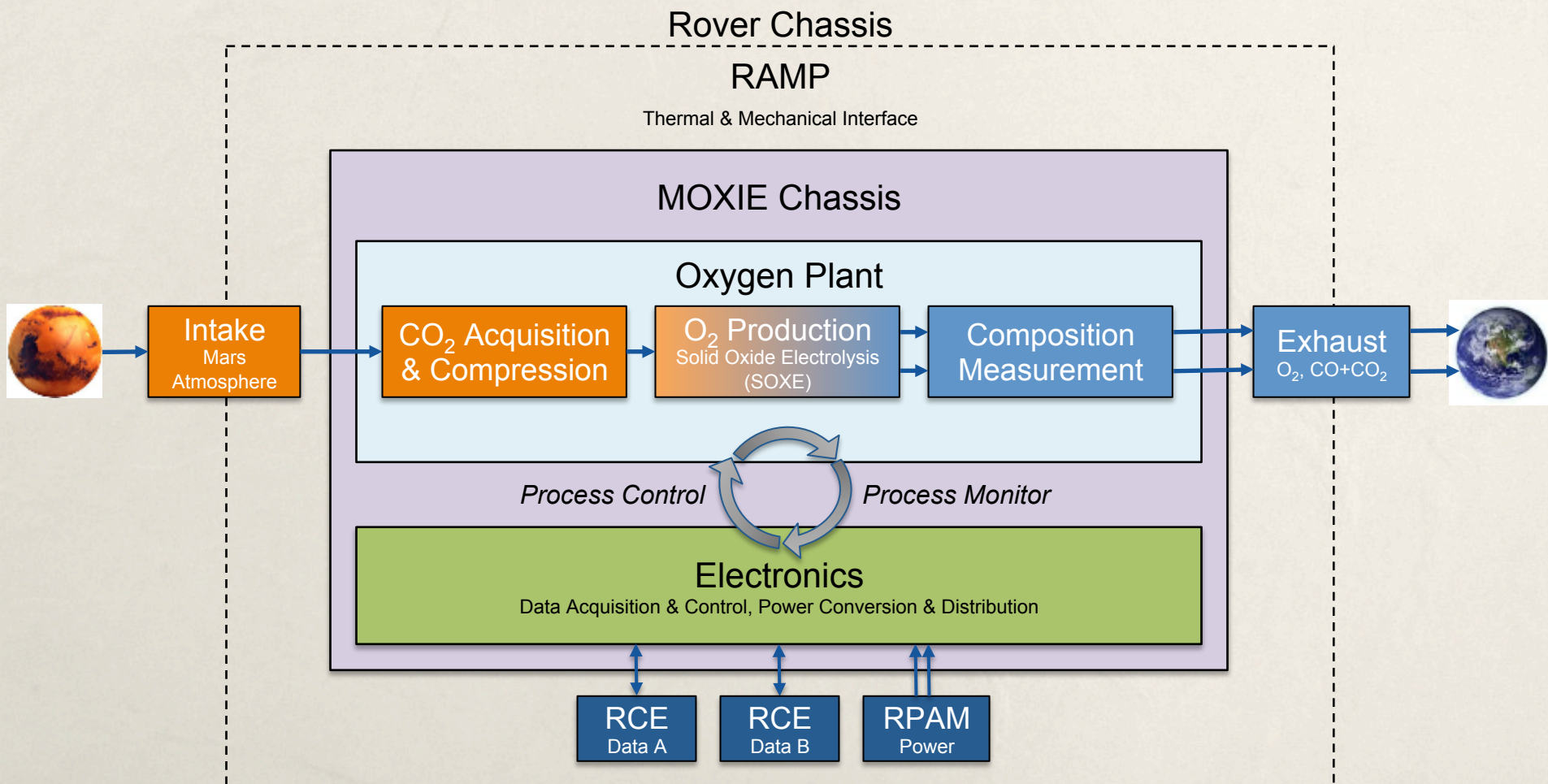




# MOXIE Functional Block Diagram



Mars 2020 Project





# Uncertainties in production rate



- \* MOXIE production rate is a balance of:
  - \* SOXE capability
  - \* Pump capability
  - \* Power supply capability
  - \* Safe operating conditions (**TBD**)
  - \* Landing site (**TBD**)
  - \* Season and time of day

# Landing site characteristics



- \* Potential landing site elevations and pressure
  - \* **Planet average:** ~4.6 Torr, but not really relevant (see below)
  - \* **Elevation:** Varies over *many* kilometers, dominated by hemispheric dichotomy. *Corresponding surface pressure varies by more than  $\times 2$ .*
- \* Likely landing sites
  - \* **Prior to M2020:** Lowlands favored for EDL. MSL, Viking < -3.6 km.
  - \* **M2020:** Sites considered between -2.6 and -0.6 km
  - \* **Human landing:** For EDL reasons, almost certain to be < -3.5 km.
- \* Types of pressure variation the rover will experience:
  - \* **Seasonal:** Up to 30% due to polar deposition of CO<sub>2</sub> (predictable)
  - \* **Diurnal:** 5-12% depending on topography (predictable)
  - \* **Weather:** A few % typically, up to 12% increase in global dust storms
  - \* **Local topography:** Several %, but below resolution of GCM





|    | A     | B                                                                  | C        | D        | E         | K                      | L        | M       | N        | O      | R             | S      |
|----|-------|--------------------------------------------------------------------|----------|----------|-----------|------------------------|----------|---------|----------|--------|---------------|--------|
| 1  |       |                                                                    |          |          | MOLA      | GCM (Forget et al) [2] |          |         |          |        | VL1-based [3] |        |
| 2  |       |                                                                    | Lat      | Long     | Elevation | Ls 150                 |          | Ls 260  |          | Max*   | Low           | High   |
| 3  | #     |                                                                    | (deg N)  | deg (E)  | (m)       | Low (T)                | High (T) | Low (T) | High (T) | (Torr) | (Torr)        | (Torr) |
| 4  | 7     | Nili Fossae                                                        | 21.097   | 74.3494  | -655      | 3.89                   | 4.12     | 4.84    | 5.18     | 5.72   | 3.76          | 5.63   |
| 5  |       | E. Margaritifer [b]                                                | -5.596   | 353.835  | -1249     | 3.98                   | 4.27     | 4.87    | 5.33     | 5.78   |               |        |
| 6  | 2     | Eberswalde [a]                                                     | -23.7749 | -33.5147 | -1400     | 4.19                   | 4.57     | 4.85    | 5.32     | 5.74   | 4.04          | 6.06   |
| 7  |       | Nili Carbonate [b]                                                 | 21.7     | 78.9     | -1458     | 4.19                   | 4.29     | 5.32    | 5.51     | 6.14   |               |        |
| 8  | 8     | SW Melas                                                           | -9.8132  | -76.4679 | -1886     | 4.19                   | 4.61     | 5.02    | 5.57     | 6.17   | 4.23          | 6.34   |
| 9  | 1     | Columbia Hills [a]                                                 | -14.5478 | 175.6255 | -1900     | 4.22                   | 4.62     | 5.17    | 5.79     | 6.22   | 4.23          | 6.34   |
| 10 | 6     | NE Syrtis                                                          | 17.8889  | 77.1599  | -2035     | 4.36                   | 4.52     | 5.57    | 5.82     | 6.53   | 4.27          | 6.40   |
| 11 | 3     | Holden Crater                                                      | -26.62   | -34.8713 | -2129     | 4.42                   | 4.89     | 5.03    | 5.57     | 5.99   | 4.30          | 6.46   |
| 12 | 5     | Mawrth Valles                                                      | 23.9685  | -19.0609 | -2247     | 4.45                   | 4.58     | 5.67    | 5.93     | 6.50   | 4.38          | 6.58   |
| 13 | 9     | Hypanis Valles [a,c]                                               | 11.8     | 314.6    | -2600     | 4.59                   | 4.81     | 5.84    | 6.22     | 6.92   |               |        |
| 14 | 4     | Jezero Crater                                                      | 18.4386  | 77.5031  | -2620     | 4.57                   | 4.76     | 5.85    | 6.14     | 6.90   | 4.50          | 6.76   |
| 15 |       | VL-1 [1]                                                           | 22.48    | -49.79   | -3627     | 4.82                   | 4.98     | 6.17    | 6.54     | 7.30   |               |        |
| 16 |       | MSL (Landing)**                                                    | -4.59    | 137.44   | -4400     | 5.22                   | 5.70     | 6.50    | 7.28     | 8.00   |               |        |
| 17 |       | VL-2 [1]                                                           | 47.97    | -225.47  | -4505     | 5.49                   | 5.58     | 7.41    | 7.61     | 8.28   |               |        |
| 18 | 10    | McLaughlin Crater [c]                                              | 21.818   | 337.749  | -5028     | 5.60                   | 5.86     | 7.32    | 7.76     | 8.45   |               |        |
| 19 |       |                                                                    |          |          |           |                        |          |         |          |        |               |        |
| 20 | Notes |                                                                    |          |          |           |                        |          |         |          |        |               |        |
| 21 | *     | "Dust Storm Max Solar" mode.                                       |          |          |           |                        |          |         |          |        |               |        |
| 22 | **    | Now at -4292                                                       |          |          |           |                        |          |         |          |        |               |        |
| 23 | [a]   | Added at 2nd workshop                                              |          |          |           |                        |          |         |          |        |               |        |
| 24 | [b]   | Eliminated after 2nd workshop                                      |          |          |           |                        |          |         |          |        |               |        |
| 25 | [c]   | Under consideration for science assessment only.                   |          |          |           |                        |          |         |          |        |               |        |
| 26 |       |                                                                    |          |          |           |                        |          |         |          |        |               |        |
| 27 | [1]   | Smith, D.E. et al, J. Geophys. Res. 106, 23689 (2001)              |          |          |           |                        |          |         |          |        |               |        |
| 28 | [2]   | http://www-mars.lmd.jussieu.fr/mcd_python/. "Climatology Ave" mode |          |          |           |                        |          |         |          |        |               |        |
| 29 | [3]   | From Mike Mischna                                                  |          |          |           |                        |          |         |          |        |               |        |

# Considerations in eventual design



- \* Where do we land? Weigh *perceived* science value against:
  - \* Ready availability of water ice (i.e. high latitude)
  - \* Safety/ease of landing (low elevation, maybe low latitude)
  - \* Surface traverse capability
- \* Assuming low latitude (no ice)... what limits performance? What infrastructure is available?
  - \* Human base will likely need nuclear reactor → plentiful power during ISRU stage
  - \* Oxygen storage will likely need cryogenics → may as well use it for other systems, e.g.
    - \* Parallel, out-of-phase cryogenic CO<sub>2</sub> acquisition instead of pump.
    - \* Separation of Ar, N<sub>2</sub> for buffer gases in habitat.
    - \* Further purification of breathable O<sub>2</sub>.
- \* Assuming high latitude, ready ice availability...
  - \* Do we want to do CO<sub>2</sub> ISRU at all?



# Pump constraints



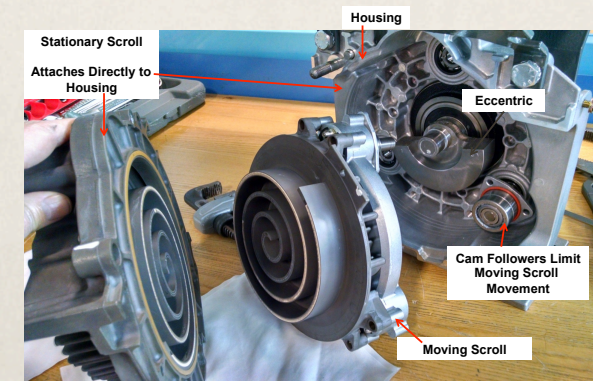
## \* Things we can estimate:

- \* *Reference performance: 79 g/hr* for inlet gas  $P=7.6$  Torr,  $T=20^{\circ}\text{C}$ .
- \* *Ambient pressure and temperature modulation:* Varies predictably with season, time of day, and to a small extent, weather.
- \* *Pressure drop from ambient to pump inlet:*  $<10\%$  (ignoring dust)

## \* Things we don't yet know

- \* Where we will land
- \* Safe  $\text{CO}_2$  utilization factor (tested 30%, probably ok at 50%)
- \* Heating of gas from outside to pump inlet (so we'll assume  $20^{\circ}\text{C}$ ).

*The MOXIE scroll compressor is under development by  
Air Squared, Inc., Broomfield, CO*





# Pump Trades and extensibility

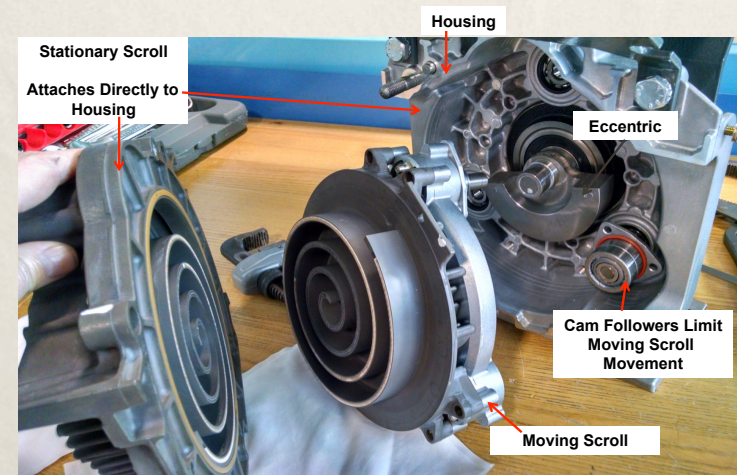


## ★ Trade for MOXIE

- ★ Scroll pump was found to be the only feasible approach on a small scale that can do real time compression without intermediate storage.

## ★ Trade for full-scale mission

- ★ Scroll pump can be scaled at least 10-fold, is energy-efficient, and lifetime should be adequate.
- ★ Cryogenic options may be more favorable if cryogenic subsystem is used for O<sub>2</sub> storage. Energy may not be a factor.





# SOXE Constraints



## \* Things we know

- \* Area ( $22.7 \text{ cm}^2$ ) and number of cells (10)
- \* Power supply limit: 4A, 35W.

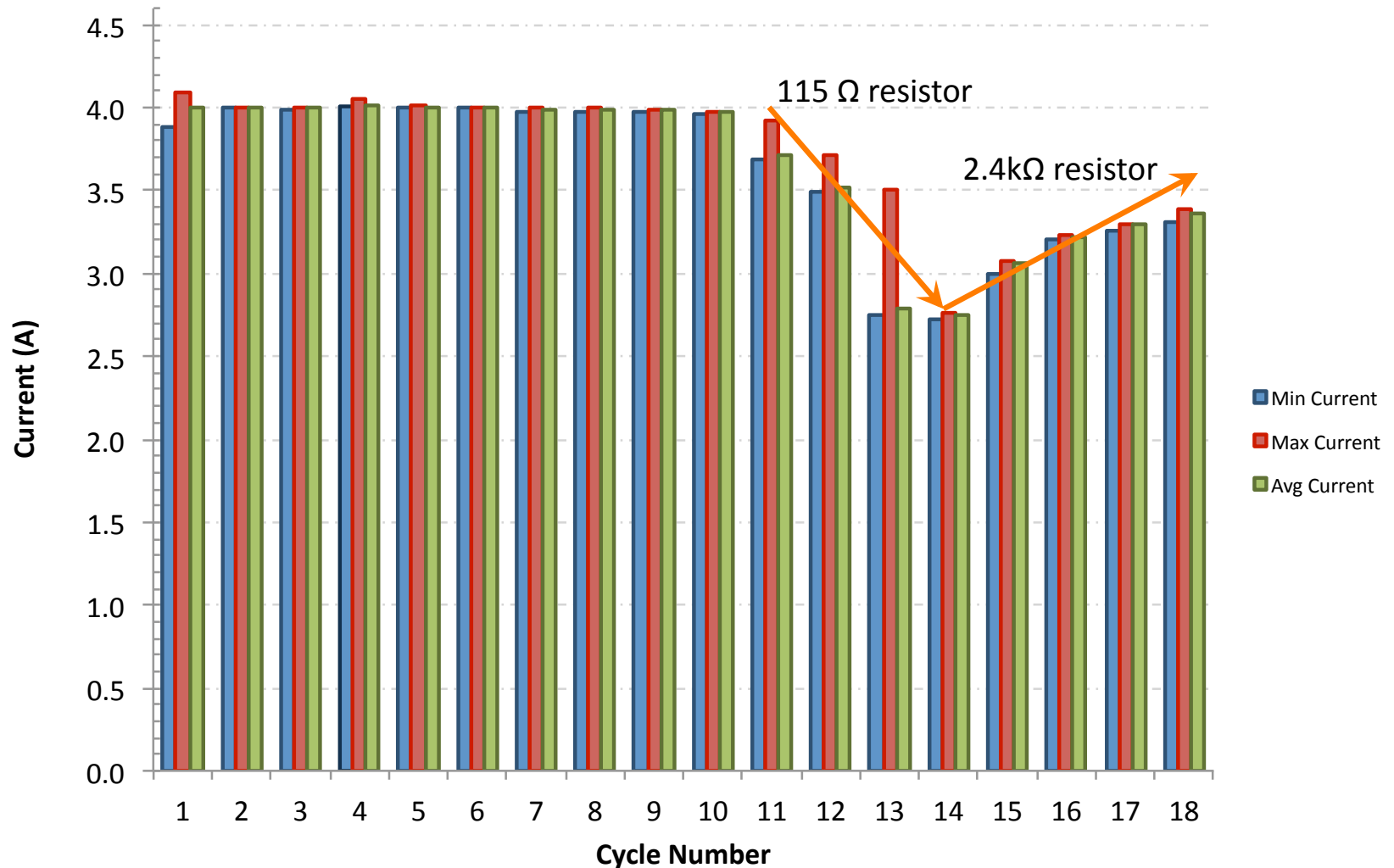
## \* Things we can estimate

- \* *Starting ASR*:  $\sim 2.5 \text{ } \Omega\text{-cm}^2$  after a few test cycles
- \* OCV:  $\sim 0.8\text{V}$
- \* *Observed degradation*:  $\sim 0.1 \text{ } \Omega\text{-cm}^2$  per cycle.

## \* Things we don't know yet

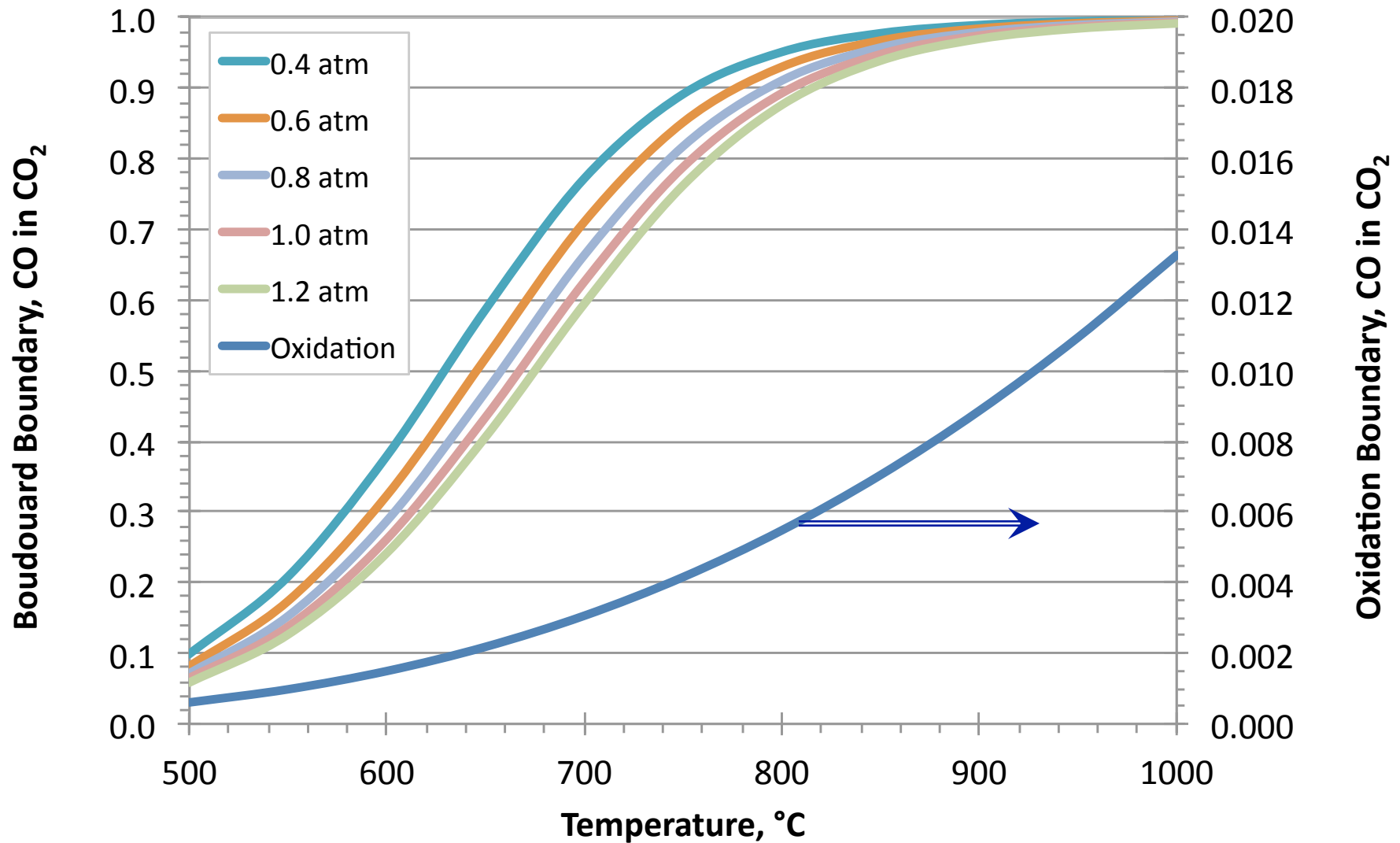
- \* *Safe operating voltage*. Presumed somewhere between 1.2V (test condition) and 1.46V (thermal neutral).
- \* *Safe  $\text{CO}_2$  utilization fraction*: We have run up to 60%. Currently running at 30%. General sense is that 50% is probably ok.

# Stability with heat/cool cycling & test of intentional oxidation from power supply leakage





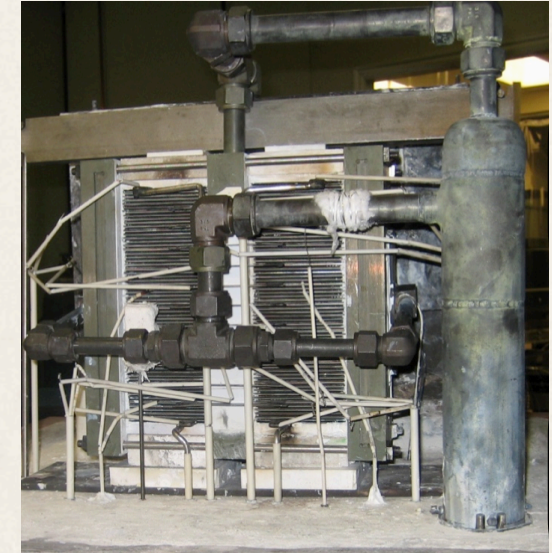
# Boudouard and Ni Oxidation Limits



# SOXE extensibility

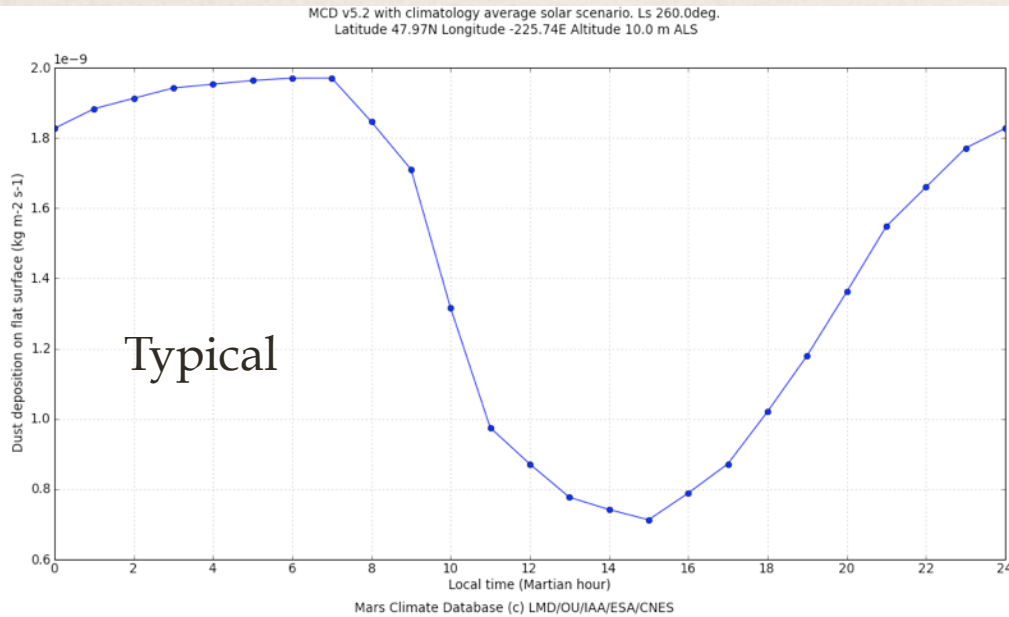


- \* MOXIE is intended to be ~1% scale model of eventual human-scale system
- \* SOXE is readily scalable by increasing # of stacks.
- \* Indications are that lifetime is acceptable but more tests needed.
- \* May want to cascade stacks to utilize “waste”  $\text{CO}_2$





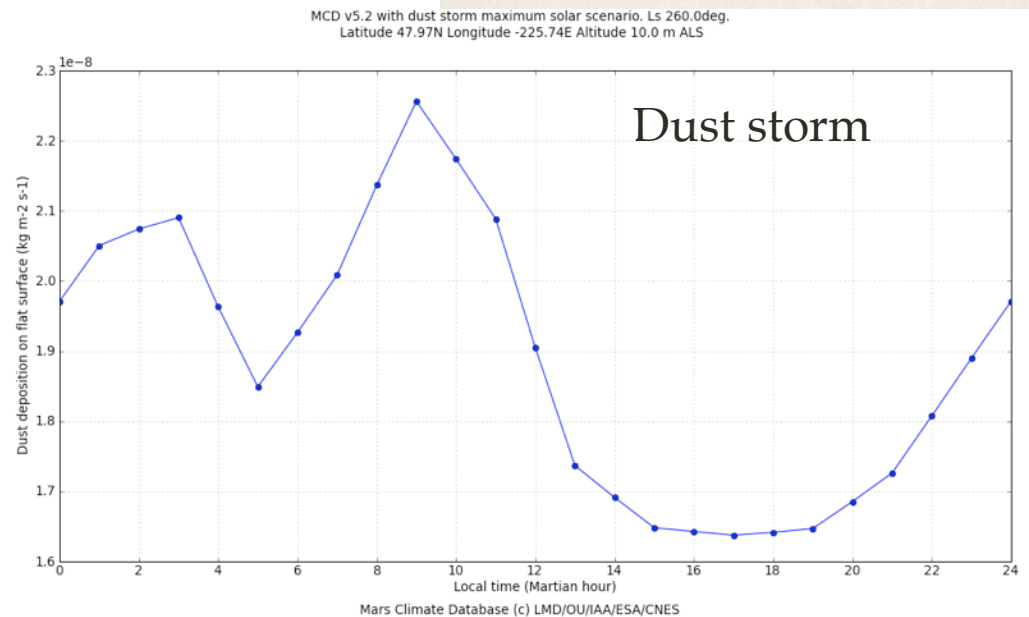
# Dust deposition rates



Peak  $2 \times 10^{-9}$

*Deposition ( $\text{kg/m}^2\text{-s}$ ) over  
the course of a day at  
Ls=260, VL-2 site*

Peak  $2.3 \times 10^{-8}$



# Questions?

